

# ICME Guided Development of Advanced Cast Aluminum Alloys For Automotive Engine Applications

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Project ID: MAT060

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2018 DOE VEHICLE TECHNOLOGY PROGRAM REVIEW



# Overview

## Timeline

- Project start date: February 2013
- Project end date: August 2018
- Percent complete: 100%

## Barrier

- High temperature performance
- Design data & modeling tools
- Manufacturability
- Cost

## Budget

- Total project funding
  - DOE share: \$3.24M
  - Contractor share: \$1.39M
- Funding received in FY17
  - \$716K
- Funding for FY18
  - \$0

## Partners

- Alcoa Inc.
- Nemak
- MAGMA Foundry Technologies, Inc.
- University of Michigan



# Project Objectives

- To develop a new class of advanced, cost competitive aluminum casting alloys providing a 25% improvement in component strength relative to components made with A319 or A356 alloys for high-performance engine applications.
- To demonstrate the power of Integrated Computational Materials Engineering (ICME) tools for accelerating the development of new materials and processing techniques, as well as to identify the gaps in ICME capabilities.
- To develop comprehensive cost models to ensure that components manufactured with these new alloys do not exceed 110% of the cost using incumbent alloys A319 or A356.
- To develop a technology transfer and commercialization plan for deployment of these new alloys in automotive engine applications.



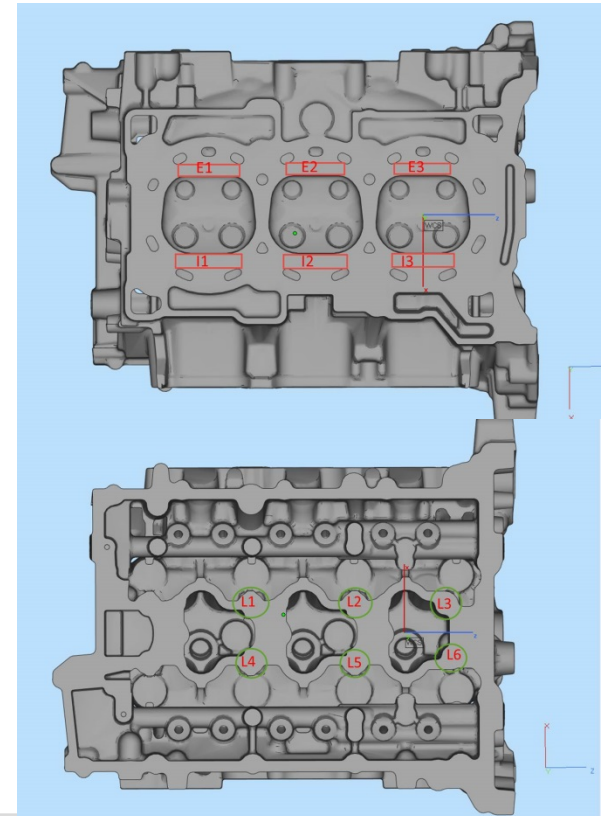
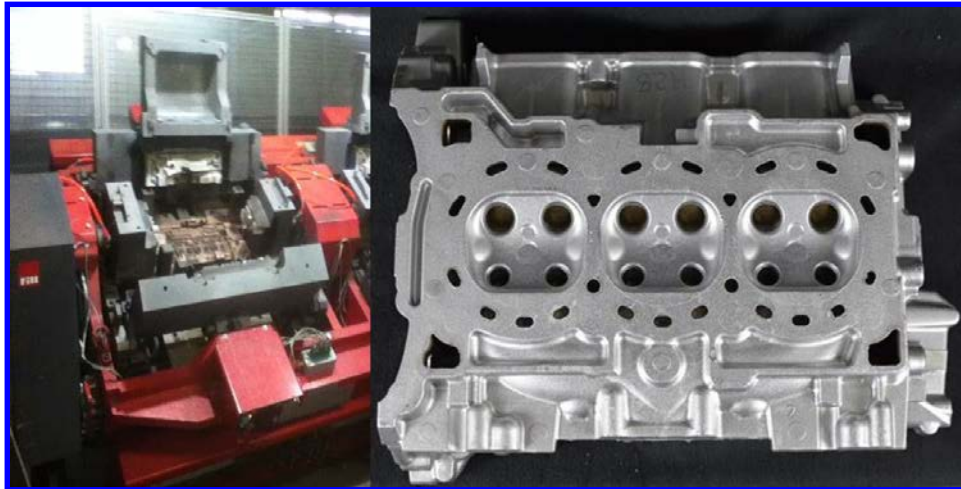
# Outline

- Alloy Design Approach
- Experiments
  - Microstructure Characterization
  - Mechanical Properties
- **Prototyping**
  - 1.5L GTDI Dragon Heads
  - 2.0L GTDI Duratec Bearing Beam
- **ICME Tools Development and Gap Identification**
  - Solidification
  - Solution treatment
  - Precipitates kinetics
  - Casting process simulation
- **Cost Model Development**
- **Summary**



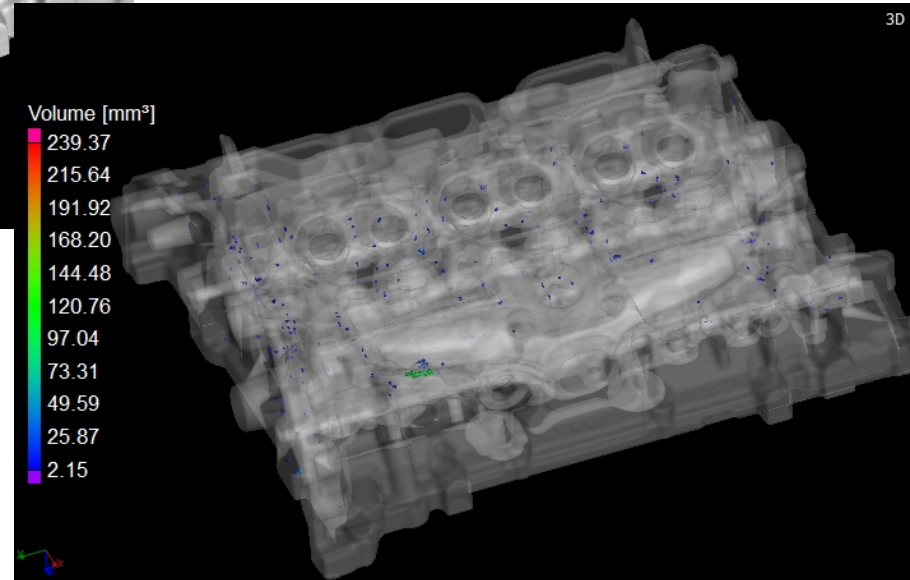
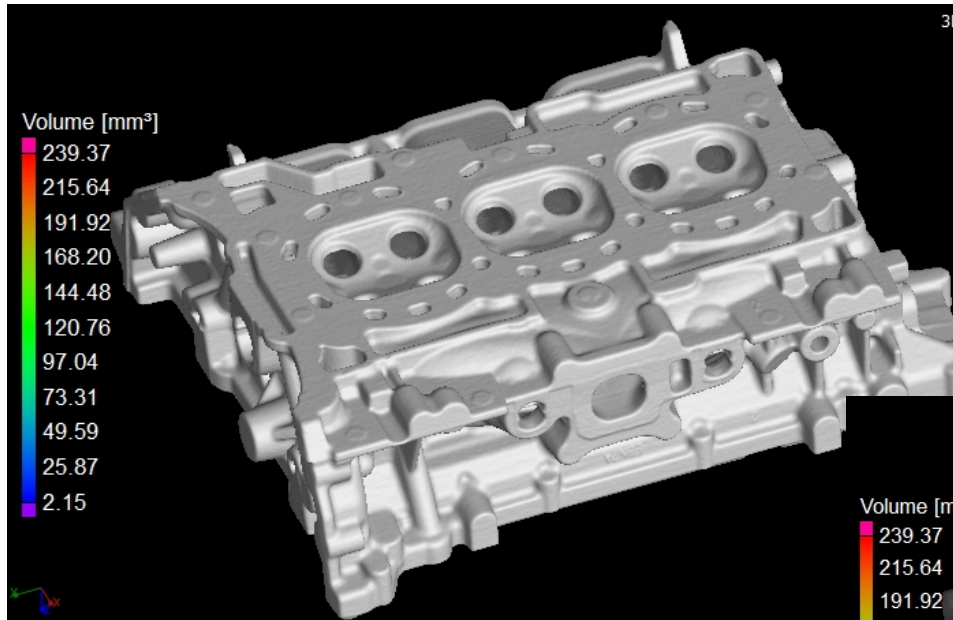
# Prototyping: 1.5L GTDI Dragon Heads

- Prototyping : conducted at Qin'an, China
- Alloys: AS7GU, Alcoa C3A1 and two Ford new alloys
- Castings: 50 castings per composition
- Sample locations: Deck Face with fast solidification rate, and Bolt Boss with slow solidification rate



# Prototyping: 1.5L GTDI Dragon Heads

- Castability verified by CT scan



# Prototyping: 2.0L GTDI Duratec Bearing Beam

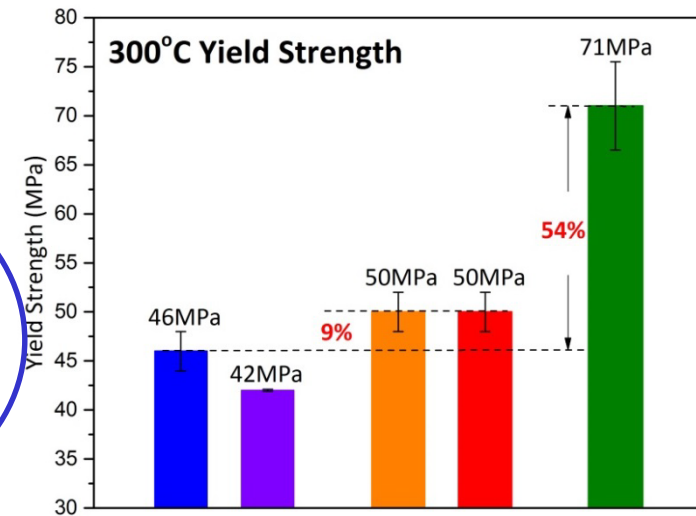
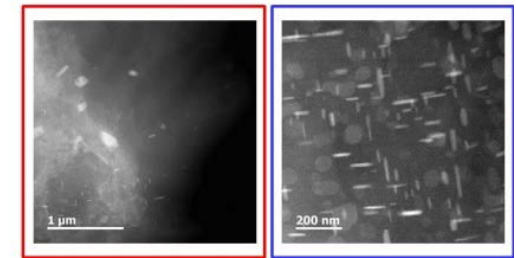
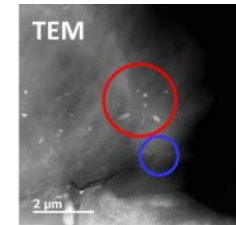
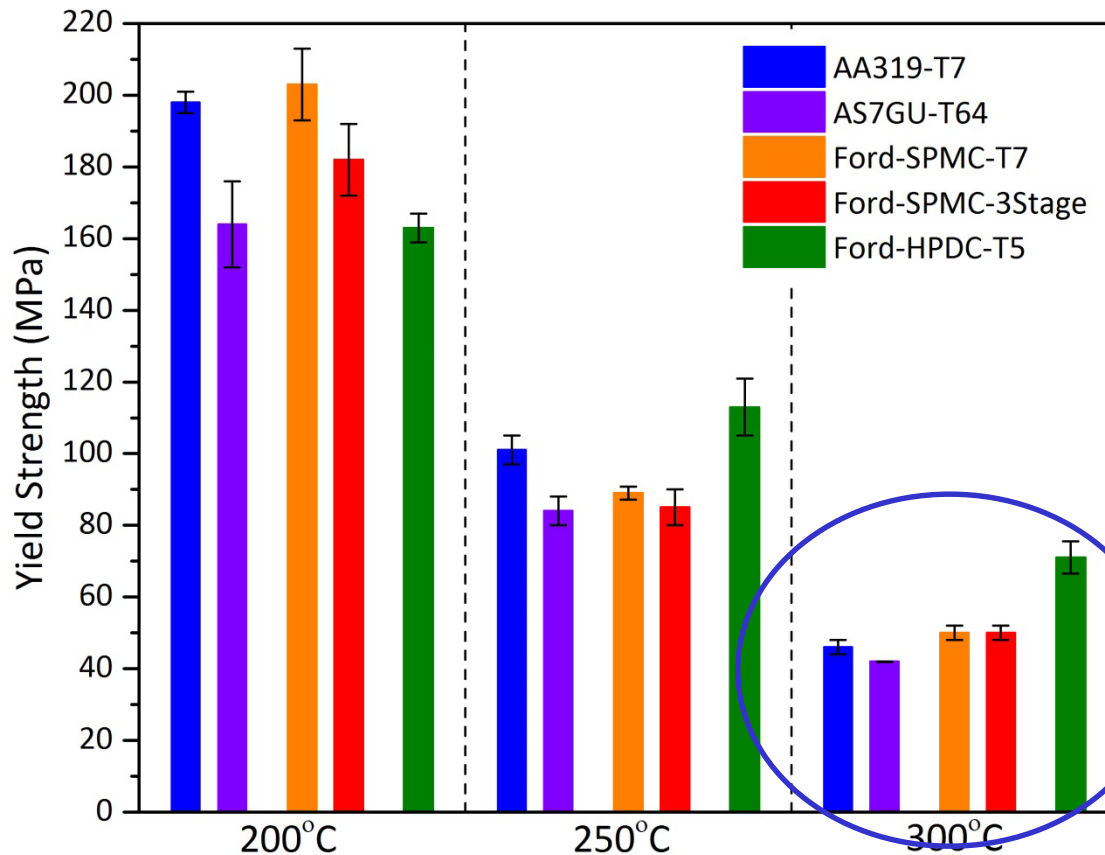
- Prototyping was conducted at Mag-tec, Jackson, MI
- Alloys: ADC12Z, Alcoa C667F and Ford-HPDC
- Castings: 200 Bearing Beams for each composition
- Sample locations: 5 locations for each Bearing Beam





# Experiments: Elevated Temperature Tensile Properties

High-temperature quasi-static yield strength showing improved mechanical properties in Ford engine application alloys

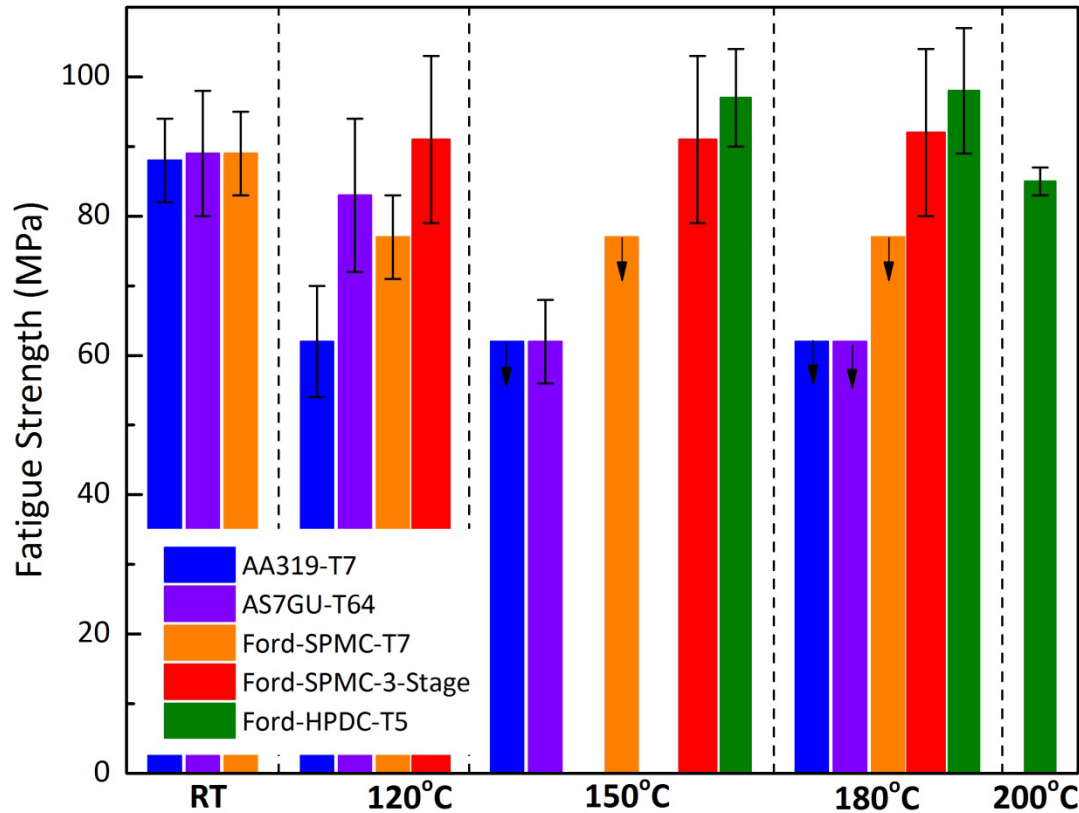




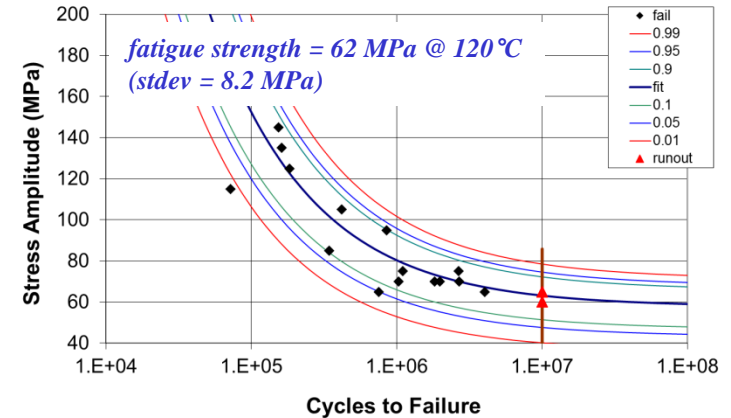
# Experiments: Elevated Temperature Endurance Limit

Industry-first superior high-temperature high-cycle fatigue strength (>90MPa at 180°C) allows Ford to significantly advance engine design and performance and reduce TGWs

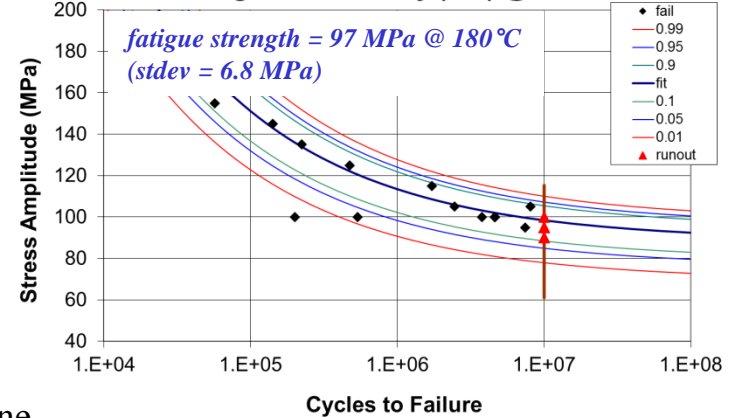
High-Cycle Fatigue Tests at Different Temperatures



Cylinder head alloy AA319-T7 @ 120°C



Ford engine block alloy (-T5) @ 180°C



Patent application, “Advanced Cast Aluminum Alloys for Automotive Engine Application with Superior High-Temperature Properties,” filed on July 28, 2017.



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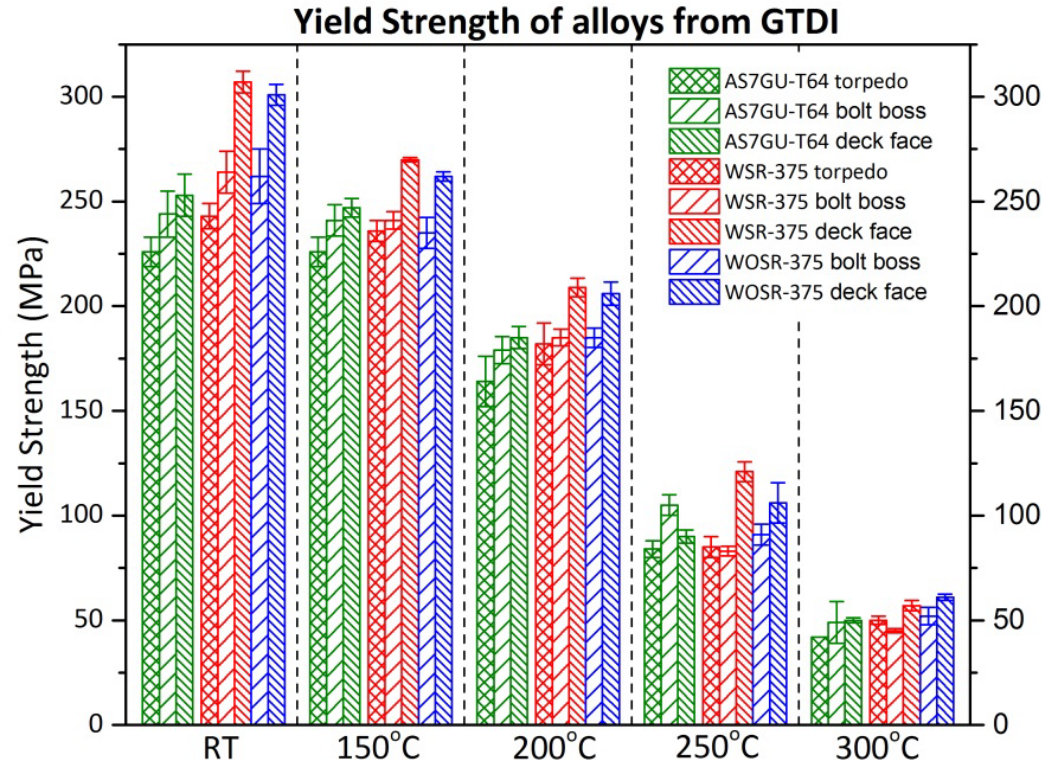
# Prototyping: 1.5L GTDI Dragon Heads

- **Yield strength (YS) and ultimate tensile strength (UTS)**

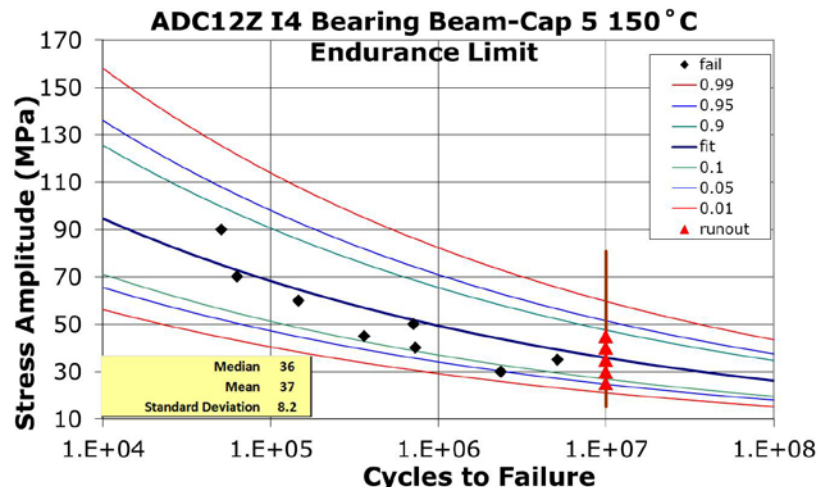
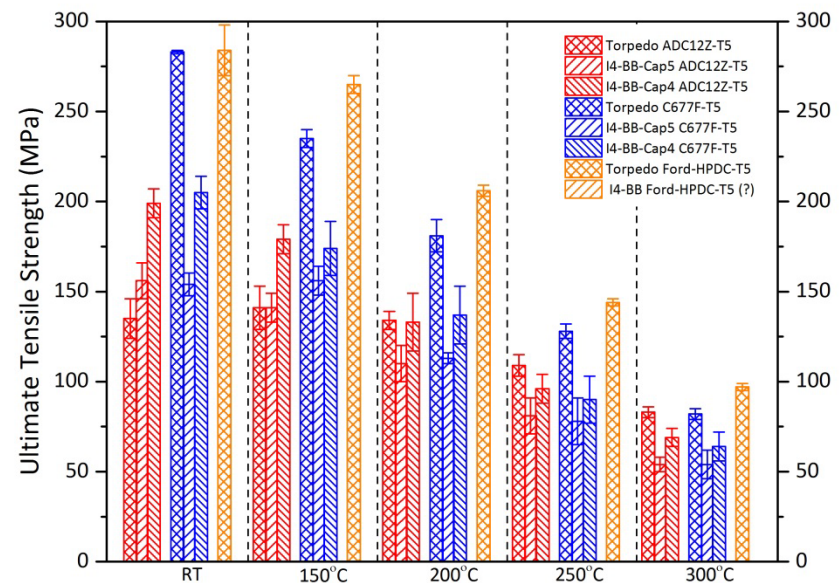
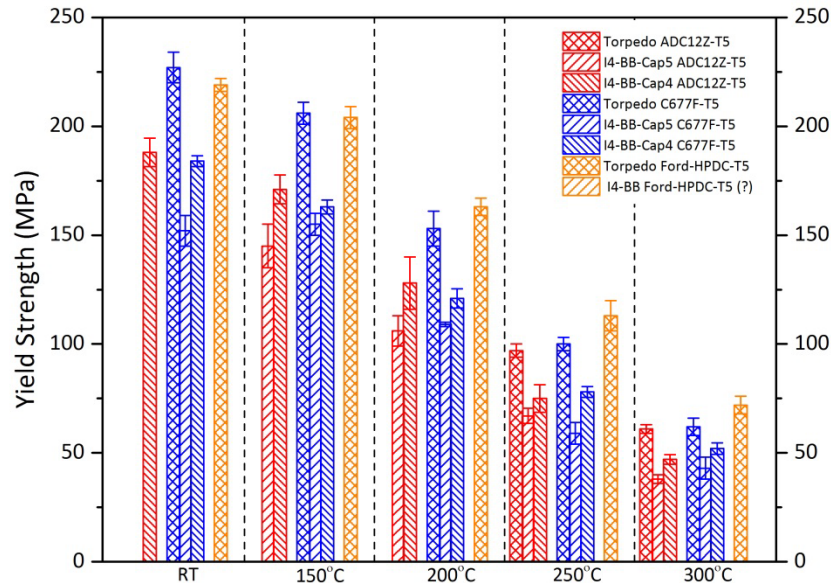
- Deck face > Bolt boss  $\approx$  test casting
- Deck face: Ford new alloys > AS7GU
- Bolt boss: Ford new alloys  $\approx$  AS7GU

- **High cycle fatigue (HCF)**

- HCF at 150°C:  
Ford new alloy  $\approx$  AS7GU  
( $\sim 93\text{MPa}$ )
- HCF at 180°C: Ford new alloy > AS7GU



# Prototyping: 2.0L GTDI Duratec Bearing Beam



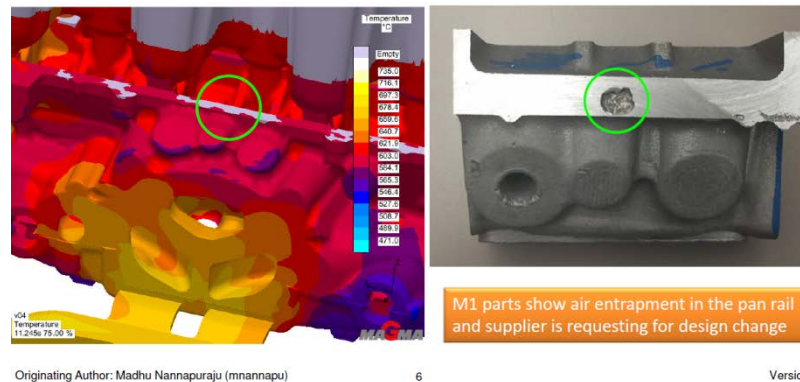
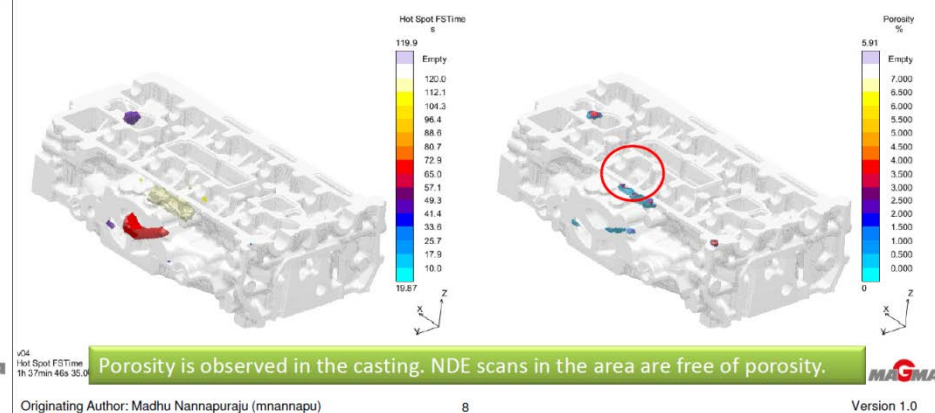
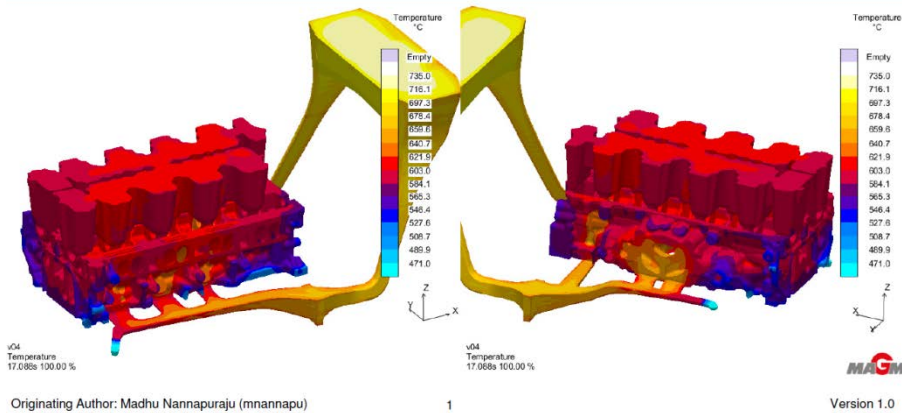
- Low mechanical properties due to high level porosity
- Ryobi 380 is still below 40MPa
- HPDC castings at Ryobi at Japan





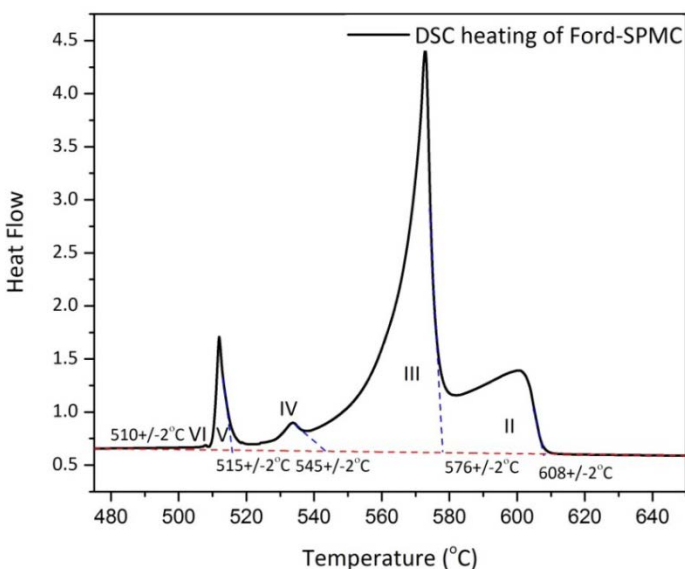
# Computational Tools Evaluation: Casting Process Sim.

- MagmaSoft is used to simulate the casting processes
  - GTDI Dragon Head, GTDI Duratec Bearing Beam, and Scorpion Head
  - Magmasoft has the full capability in casting process simulation



# Computational Tools Evaluation: Solidification

- Scheil Model predicted phase transition temperatures and solid phase fractions
- Phase transition temperatures & relative phase fractions can be measured by DSC
- Gap analysis: Scheil model predicted phase transition temperatures are off from DSC measurement



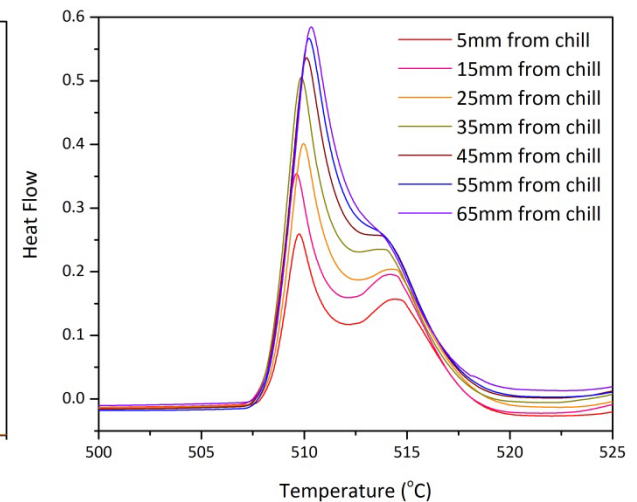
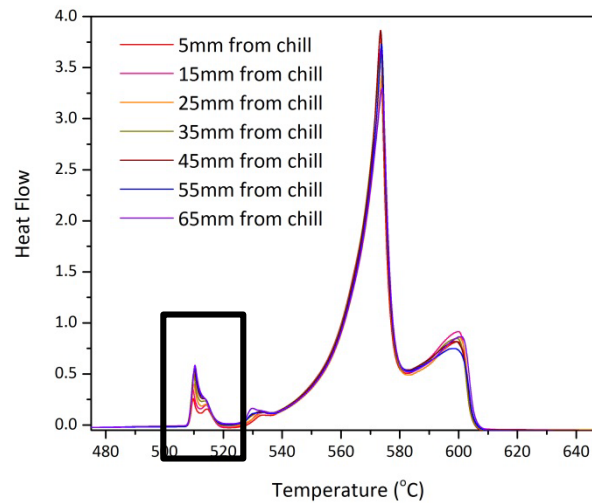
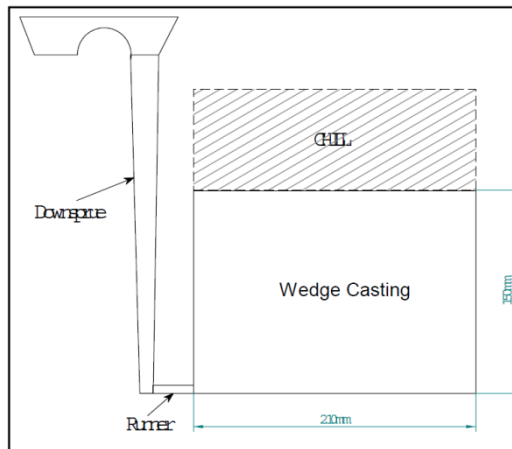
Temperature measured in DSC (°C)	Temperature predicted In Scheil (°C)	Difference (°C)	Formed Phases
N/A	690	N/A	D0 <sub>22</sub> /D0 <sub>23</sub>
608±2	591	17	Fcc_a1
576±2	557	19	Diamond_a4
545±2	515	30	Al9Fe2Si2
515±2	510	5	Al2Cu_C16
510±2	510	0	Q-AlCuMgSi



# Computational Tools Evaluation: Solidification

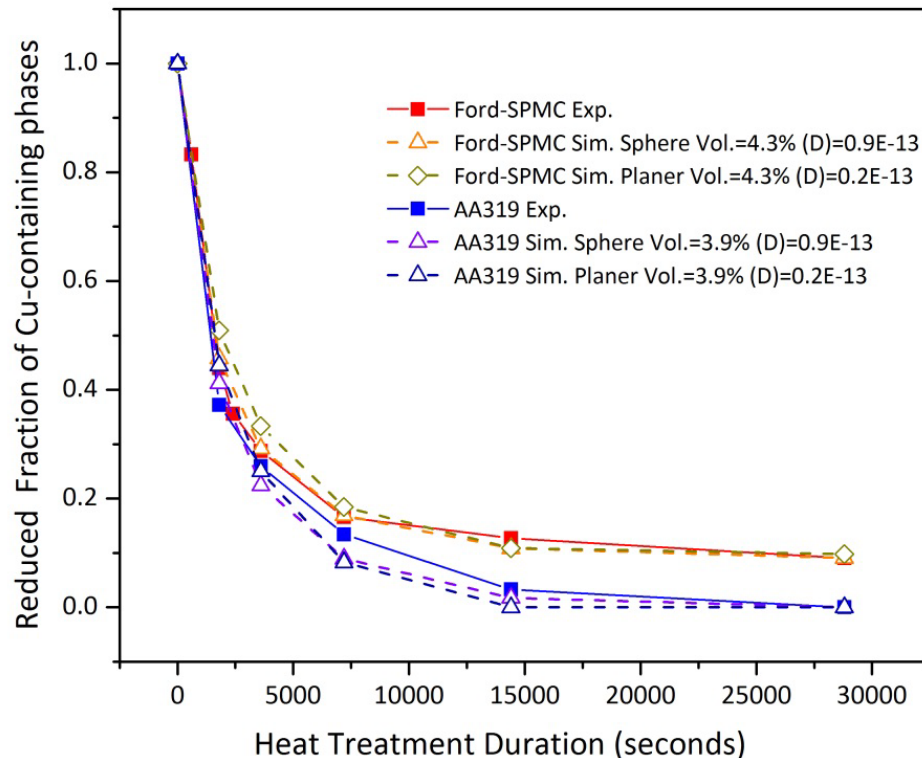
- DSC measurement shows the fraction of Theta\_AlCu increases with decreasing of cooling rates
- The fraction of theta\_AlCu in Scheil doesn't change with cooling rates
- Gap of Scheil Model: no cooling rates effect in considered in Scheil model

Solid phases fraction						
D0 <sub>22</sub>	D0 <sub>23</sub>	fcc_a1	Diamond_a4	Al9Fe2Si2	Al2Cu_C16	Q_AlCuMgSi
0.28	0.57	86.82	6.16	0.58	5.02	0.56



# Computational Tools Evaluation: Solution Treatment

- Reduce fraction is easy to obtain through simulation
- Simulated results show good agreement with DSC results
- Gap Identification:
  - More reasonable geometry (cylinder and sphere2)
  - Zr and V can not be included in calculation
  - Optimization of mobility database





# Computational Tools Evaluation: Spherical Precipitates

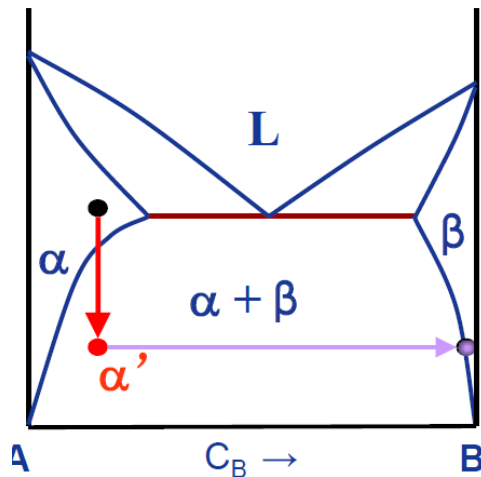
- Kampmann and Wagner numerical method to solve Langer-Schwartz

problem:

1<sup>st</sup> stage: Classic Nucleation Theory-  
homogeneous or inhomogeneous

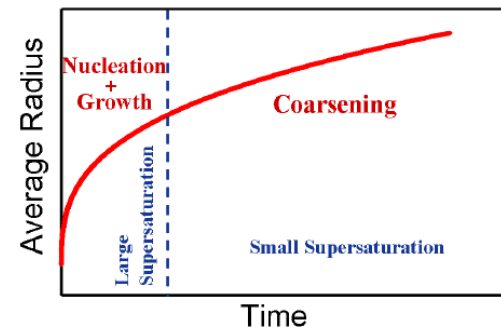
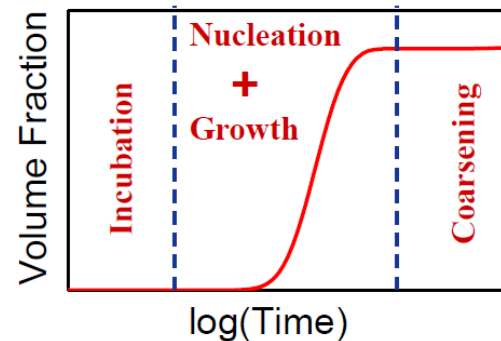
○  $\frac{\partial f(r,t)}{\partial t} = -\frac{\partial}{\partial r} [v(r)f(r,t)] + j(r,t)$  2<sup>nd</sup> stage : Diffusion controlled continuity equation-  
Binary model, PrecipiCalc model, *et al*

○  $C_0^\alpha = C^\alpha + (C^\beta - C^\alpha) \int_0^\infty \frac{4\pi}{3} f(r,t) r^3 dr$  3<sup>rd</sup> stage: Coarsening after  $j(r,t)$   
disappears: LSW model



' : matrix phase (supersaturated )  
precipitate phase

: stable solid solution

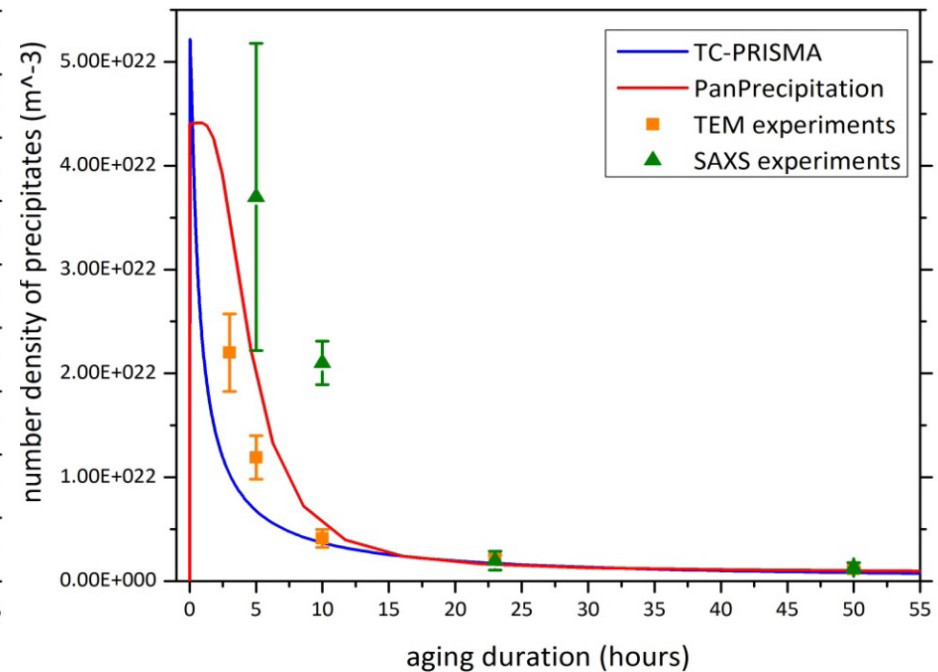
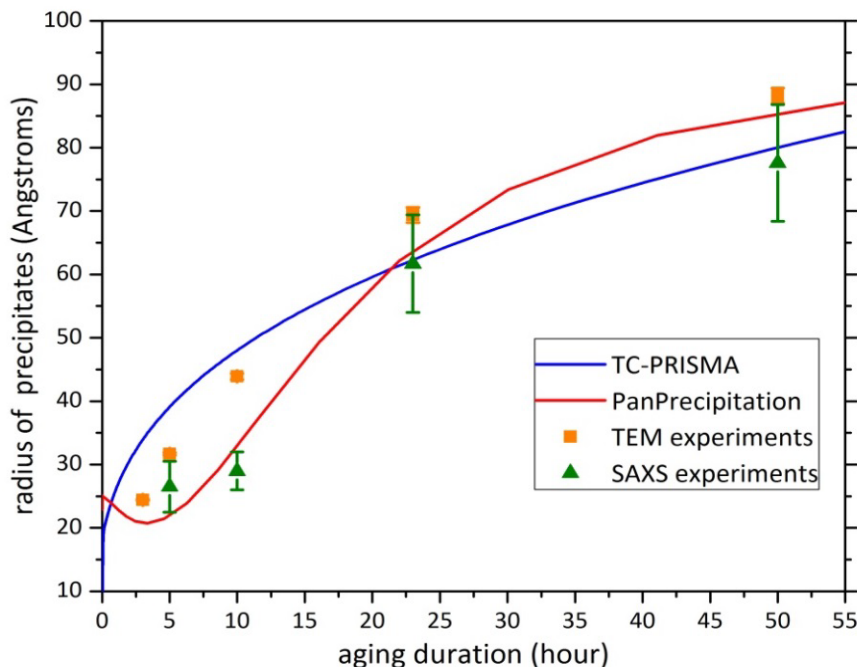


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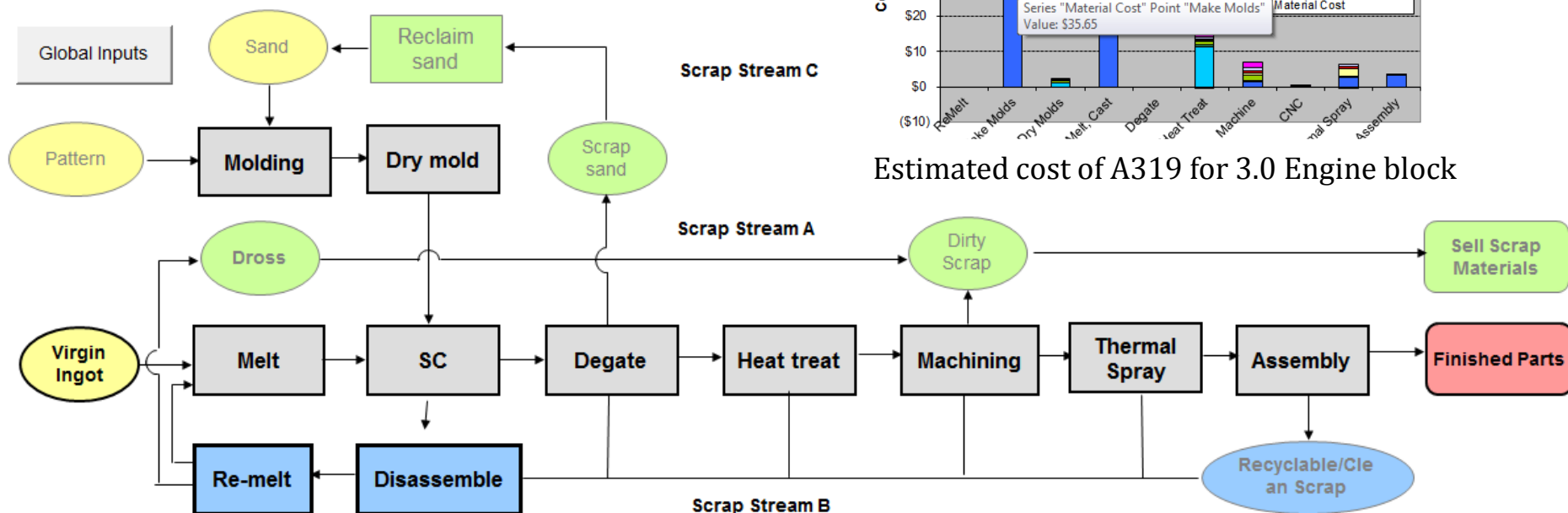
# Computational Tools Evaluation: Spherical Precipitates

- PanPrecipitation from CompuTherm and TC-PRISMA from Thermo-Calc
- Thermodynamic database: TCAL5 and PanAl2016
- Mobility database: MOBAL3 and PanAl2016
- Kinetic databases are developed: Interfacial energy, strain energy nucleation site parameter, molar volume
- An enhance mobility parameter is added: Si can accelerate the kinetics of L12-Al<sub>3</sub>Zr Precipitates



## A sand casting cost model has been developed at Ford

- 
- Manufacturing Cost Breakdown - by Operation**
- Cost (\$/pc)
- Series "Material Cost" Point "Make Molds" Value: \$35.65
- Legend:
- Cost of Capital
  - Overhead Labor Cost
  - Maintenance Cost
  - Building Cost
  - Tooling Cost
  - Equipment Cost
  - Utility Cost
  - Direct Labor Cost
  - Material Cost
  - Material Cost
- | Operation     | Material Cost | Direct Labor Cost | Utility Cost | Equipment Cost | Tooling Cost | Building Cost | Maintenance Cost | Overhead Labor Cost | Cost of Capital |
|---------------|---------------|-------------------|--------------|----------------|--------------|---------------|------------------|---------------------|-----------------|
| ReMelt        | 0             | 0                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Make Molds    | 35.65         | 0                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Make Molds    | 0             | 2                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Make Molds    | 0             | 0                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Degate        | 0             | 0                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Degate        | 0             | 12                | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Machine       | 0             | 8                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| CNC           | 0             | 0                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Thermal Spray | 0             | 3                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |
| Assembly      | 0             | 3                 | 0            | 0              | 0            | 0             | 0                | 0                   | 0               |



# Conclusion

## Summary

- I. Successfully developed two novel combined alloy-heat treatment procedures for high temperature powertrain applications.**
- II. Demonstrated alloys performance on prototyped component**
- III. Evaluated several commercial ICME tools and Identify their Gaps**

